

New Developments in Surface Oil Flow Visualization

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The prolific application of digital imaging and image processing for studying flows is extended to surface oil flow visualization. The use of colored, fluorescent mixtures enable bright, high-contrast images to be obtained which facilitate image processing. Examples were provided in visualizing the surface flow past micro vortex generators. Image processing of video sequences revealed minute features that are critical in understanding the flow.

I. Introduction

SURFACE flow visualization is a well-established technique used to help in understanding flowfields, particularly complex, three-dimensional flows.¹⁻³ The technique is used in wind and water tunnels and, occasionally, in actual flight vehicles.⁴ Specifically, for high-speed blowdown tunnels, a popular visualization technique is surface oil flow or oil-dot visualization. In the former approach, a mixture consisting of a carrier fluid such as silicone oil or kerosene and a pigment such as dye, lampblack or powdered classroom chalk is painted on the surface of a test article, with different investigators having their favorite recipes. A carrier fluid such as silicone or engine oil requires a long time to thin; in other words, the time required for a surface flow pattern to be established is long, typically over 10 s. Some investigators prefer kerosene which evaporates rapidly in the low pressure environment of most blowdown tunnels. In using kerosene, the surface pattern is formed by both the thinning of the mixture and by evaporation of the carrier liquid. In oil-dot visualization, colored dots made of similar mixtures as oil flow visualization are applied on the surface. A surface pattern of discrete streaks is formed when air flows past the surface. Comparing both methods, it appears that surface oil flow visualization appears to be easier to apply than oil-dot visualization and also produces a higher resolution of the surface features. When the pigment is in the form of tiny granules, such as with ground chalk, long, thin streaks are formed which helps in interpretation of the surface features.

The surface pattern in the presence of three-dimensional separation has been the subject of much analysis over the past five decades. Primary interest has been on understanding the surface topology⁵ and on interpreting the flowfield based on the surface flow pattern and supplementary measurements.⁶⁻⁸ The ability to generate highly-resolved numerical simulations has also allowed such surface streamlines to be visualized numerically.⁹⁻¹¹ Surface flow patterns obtained experimentally and numerically have also been used in combination to further the understanding of complex flows. It is now generally accepted that the surface streaks accurately map out the skin friction pattern except the separation line. Squire showed that the thickening of the oil layer at isolated singular separation points can create error in locating separation.¹² Unsteadiness of shock-induced separation also complicates the visualization of the separation line and, to a lesser extent, the attachment line.¹³ Moreover, in so-called open separation, the separation lines may not be

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well visualized. This is because the flow velocity remains quite high which can scour much of the mixture away, leaving only a faint residue.

Surface flow visualization is generally considered to be qualitative. Perhaps topological aspects in identifying surface singularities may be considered to be quantitative. Nevertheless, the technique has been used effectively for quantifying features such as the upstream influence, separation and attachment of two- and three-dimensional shock wave/boundary-layer interactions.^{14,15} In these methods, the dried residue is lifted off the surface by a large piece of transparent adhesive tape and pressed onto paper. The features are identified and then digitized by hand.

The advent of digital imaging hardware and software has breathed new life in surface oil flow visualization. This paper describes the use of digital techniques to improve surface oil flow visualization. Specific examples are taken from studies of supersonic flow past micro vortex generators placed ahead of shock/boundary-layer interactions.

II. Experimental Details

A. Facility

The experiments were performed in a blowdown wind tunnel. The tunnel has a continuously variable Mach number range of 1.5-4 and a Reynolds number range of 60-140 million/m. The total air storage was 24.5 m³ (865 ft³) at 5.3 MPa (750 psig) which allowed for runs of as long as 90 s. For this series of experiments, the Mach number was fixed nominally at 2.45 by removing the variable Mach number feature and installing fix adaptor plates between the nozzle and the test section.¹⁶

The test section is 15.2 cm² × 81.28 cm long (6 in.² × 2.67 ft). It was outfitted with extensive optical access from both sides and from the top. Figure 1 is a CAD mockup showing a configuration with transparencies in the front half only.

B. Test Model

A boundary layer was developed naturally over a flat plate with a sharp leading edge of 15 deg. The plate spanned the test section and was 73 cm (28.75 in.) long. The flat plate was made in layers supported by a sharp-tipped rail on each side. The top layer which was the test surface was made of a number of small, thin plates (Fig. 2). These plates butted tightly against each other to form a continuous, flat surface. This modular design allows for quick configuration changes. A cavity existed below the top surface for allowing pressure tubing, transducer wiring and other elements to be fitted. The wiring and tubing were channeled to the rear to the diffuser and outside of the flat plate in a pipe. A bottom surface encased the cavity.

Other than the flat plate itself, for the present study, various shock generators could be placed at 32.4 cm (12.75 in.) from the leading edge. These shock generators included a 5 or a 16 deg compression ramp and a 12.7 mm (0.5 in.) diameter upright cylinder.

A micro-vortex generator (MVG) array was mounted ahead of the ramp. Based on the recommendations of Anderson et al.,¹⁷ for the present experiments where the boundary layer was about 34 mm thick, the array was mounted 5.2 mm (2.05 in.) ahead of the ramp. Figure 3 shows an array of five MVGs. Each MVG was 12.95 mm (0.51 in.) long and 1.57 mm (0.062 in.) high. The front of the MVG was 11.7 mm (0.46 in.) wide. The center-to-center spacing between the MVGs was 30.5 mm (1.2 in.). Two styles of MVGs were fabricated based on the designs from [18], based on the trailing edge angle of 45 or 70 deg.

C. Test Conditions

Wind tunnel conditions were monitored by a total pressure and a total temperature probe in the plenum chamber and by a static orifice near the exit of the nozzle. The test Mach number is 2.47 ± 0.005 . The total pressure is maintained at 551 ± 6 kPa (80 ± 0.9 psia). The tunnel operation is controlled by a host computer which opened the control valve to reach steady-state conditions in about 2-3 s. The blowdown operation

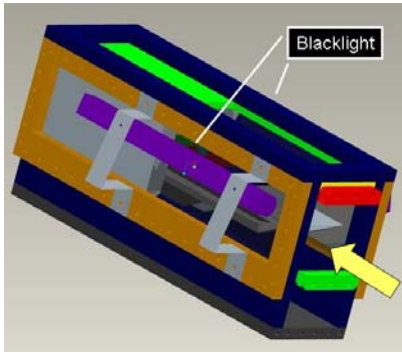


Figure 1. CAD mockup showing half transparency on the ceiling and sides. Flow from right to left.



Figure 2. Test section showing flat plate. Flow from right to left.

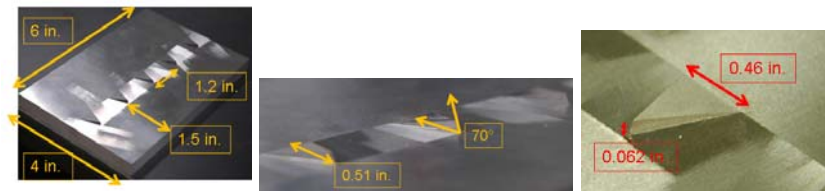


Figure 3. Micro-vortex generator array.

caused the total temperature to drop by 5 K in 30 s. Since the duration of the flow visualization experiments were less than 10 s long, the temperature drop was not significant. Thus, the unit Reynolds number can be considered to be steady at 43 million per m. Further details of the experimental setup can be found in [19].

D. Surface Flow Visualization Requirements

Reference [1] discussed in great detail the use of photographic film for recording the images. From a present-day context, the discussion reveals a number of limitations. Some of the requirements for an ideal implementation of surface flow visualization include

Bright images. Fluorescent mixture painted on a matte black surface and illuminated with diffused blacklight, with the room lights turned off.

Oil-pigment mixture. The mixture must provide sufficient spatial resolution, streaks in the surface trace, does not evaporate too soon or remain too wet that tunnel shutdown may ruin the final pattern. The temperature drop during a run which will affect the viscosity of the mixture must be also taken into account.

Minimizing error. Ideally, the camera should be placed perpendicularly to the test surface. This is achieved by extensive optical access allowing perpendicular or near perpendicular imaging.

Still and video imaging. While still images are adequate, the ability to capture video enhances the technique.

Digital image processing. Quantitative feature extraction, including the ability to track surface tracers. Accurate data require that the test surface coordinates are well established.

The surface flow visualization technique consisted of painting bands of fluorescent mixture along the surface of the plate ahead of the area of interest. (The use of fluorescent pigments with ultraviolet light in producing bright images has been reported previously, including for determining skin friction.^{1,2,20-24} Based on previous experience, a kerosene carrier evaporates readily in such test conditions to leave a dry trace within 10 s. For the present experiments, a mixture of kerosene and fluorescent chalk with a small quantity of silicone oil was found to be suitable. The exact composition required some trial and error but, generally, the mixture should have a consistency of syrup. The particle size of the ground chalk was reduced to 100 μm by straining the mixture. The small particle size improved the resolution of fine features.

A Canon Vixia HF S10 high-definition camcorder was placed perpendicularly overhead to acquire the images. This camcorder has a 2.39 megapixel (1.56 effective megapixels for video) HD CMOS sensor and frame rates of 24 or 30 per s. The maximum shutter speed, as used in the present recordings, is 1/2000 s. A still camera (Nikon D300S with a VR 18–200 mm F/3.5-5.6 lens and operated typically 1/8000 s shutter speed) was also available and can be mounted side-by-side with the video camera. The Nikon camera has a 13.1 megapixel (12.3 effective megapixel) CMOS image sensor and can capture high-definition video at 24 fps. It can be noted that the Nikon camera produces very high-resolution images that are useful for resolving small features.

“Black light” tubes (Utilitech Model Gu9721P-T8-BKI) placed on both sides of the test section were used to illuminate the mixture without turning off the ambient fluorescent lighting (Fig. 1). Figure 4 shows the bands of fluorescent mixture under black light that were applied ahead of the MVG array. Three of the MVGs that within the picture are highlighted by dashed lines. The extensive optical access in the present facility allowed the cameras to be placed perpendicularly to the test surface. This helps to minimize geometric errors. Finally, the digital processing was applied to the still or video images.

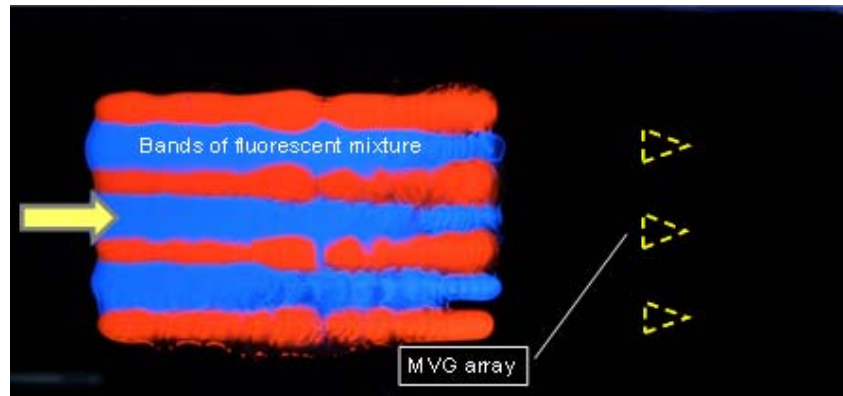


Figure 4. Bands of fluorescent mixture applied to test surface.

E. Image Processing

The emphasis here is to process video images to highlight small, obscure features. Following a review of a videoclip, the interesting segment was decompiled into individual frames using Blaze Media ProTM. The individual frames were imported into DaVisTM 7.1 which is software from LaVision for processing particle image velocimetry images.

Two nonlinear filters were used to highlight the small, obscure features. The first nonlinear filter is known as the “non-linear concentration” filter. As the paint thinned over the surface, a smoothing effect was noticed over a large range of pixels. The “non-linear concentration” filter searches for the local maximum intensity which is above a user-defined pixel noise level (set to 10 for the present purpose), and concentrates the local maximum to the center of a defined pixel area which is typically taken to be a 7×7 pixel area. The result

of this operation is to convert the color image into a high-contrast gray scale image. The second non-linear filter applied is the “non-linear subtraction sliding minimum” filter. This filter computes the local minimum over a user defined scale pixel length. This filter was chosen to further increase the contrast, whereby local maxima of intensity are made visible. Due to the precious concentration filtering process, this second process results in a pure black-and-white image, with no gray. After the image processing was completed, the images were recompiled into a video clip using Blaze Media Pro™.

III. Results and Discussion

An example of the surface flow past the bare flat plate and the MVG array is shown in Fig. 5. Figure 5(a) shows that the surface flow past the bare flat plate is mostly two-dimensional. Departures from two-dimensionality at the top and bottom of the figure are due to the way the mixture was applied. A similar remark can be made of the flow past the MVG array.

One of the image processing techniques is simply to use normal PIV vector calculations on the surface flow, treating the surface flow as if it consists of particles convecting downstream. This yielded a “surface streamline” map shown as green lines in Fig. 6. The map is superimposed on the original surface visualization, now shown in gray scale. It is clear that the surface streamlines are visualized well. There should not be any inference on surface velocity, however. While not attempted presently, it should be possible to quantify the two-dimensionality of the surface flow instead of merely suggesting that the surface flow is two dimensional visually.

Next, enlargements showing the details around an MVG are found in Fig. 7. The top view in Fig. 7(a) shows bright regions, indicating an accumulation of mixture, telltale signs that these are regions of low shear. The accumulation at the leading edge of the MVG can be readily interpreted as a region of two-dimensional separation. The fluid in the separation zone leaves from the sides, rolling up into so-called horseshoe vortices. These are regions of high shear which manifest themselves as darker regions, with the pigment being scoured away, as also observed by others.^{25,26}

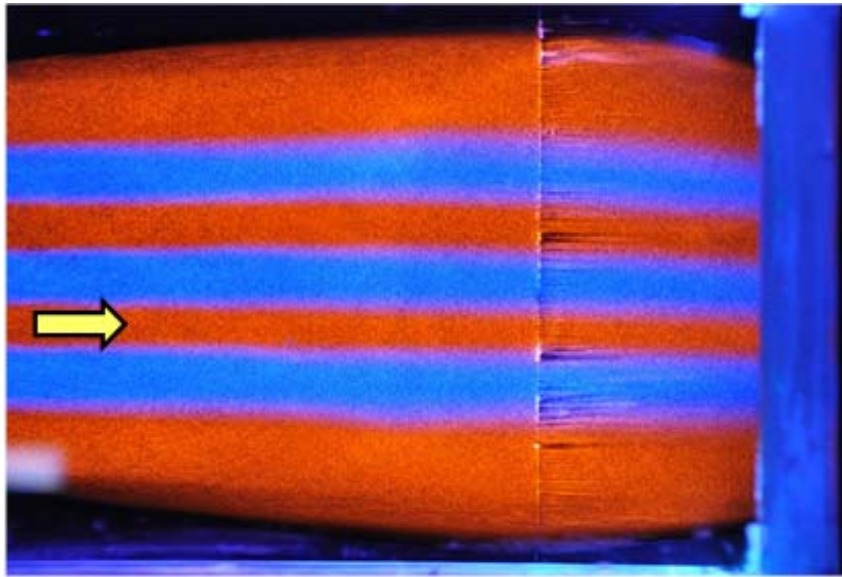
Figure 7(a) also shows accumulation on the side edges of the MVG and in a pair of long streaks on the flat plate behind the MVG. These require careful interpretation but cannot be achieved with the view directly overhead. Instead, the side view of Fig. 7(b) shows that there are in fact two regions of low shear on the side, one near the top edge of the MVG and the other at the junction of the MVG with the flat plate; see also [25–27]. These low shear regions are separated by a region that appears devoid of pigment, indicating a region of extremely high shear. Thus, a more complex topology is now revealed that was not evident from the overhead view.

To assist in identifying the type of separation around the MVG, a differently colored pigment was applied on the flat plate adjacent to the slant surfaces as shown in Fig. 8(a) of a sequence of frames from a videoclip. The sequence shows that the mixture around the slant surfaces is blown away. This indicates a high-speed region associated with open separation. Kleine²⁸ suggests that videos enable changes to be studied. Thus, visualizing the start-up transient of the surface flow in this manner can help to understand the complex flow.

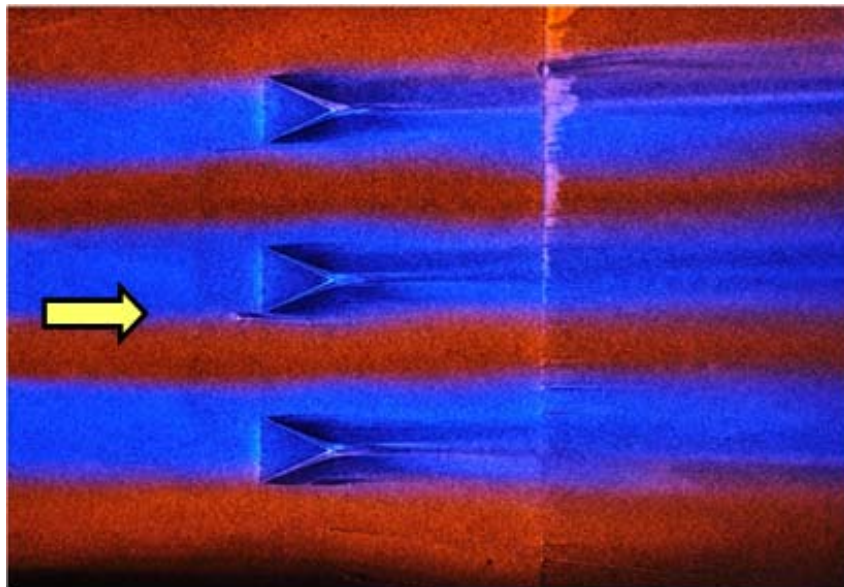
In addition, Kleine²⁸ suggests that minute features can be identified in a video that may otherwise be considered to be erroneous in a single image. In the present case, the videoclip is processed as described previously and some of the frames are shown in Fig. 9. Even though the present video is not time resolved, playing the video allows a minute but critical feature to be identified. A careful examination of Fig. 9 reveals the presence of a pair of foci which corroborates numerical evidence;²⁹ see Fig. 10 For a more detailed discussion, see [27].

IV. Conclusions

The implementation of digital imaging and image processing has revitalized surface flow visualization. The implementations were illustrated using micro vortex generators in a supersonic flow. A technique for



(a) Nominally two-dimensional surface flow past the bare flat plate.



(b) Surface flow past an MVG array.

Figure 5. Examples of color surface flow visualization.

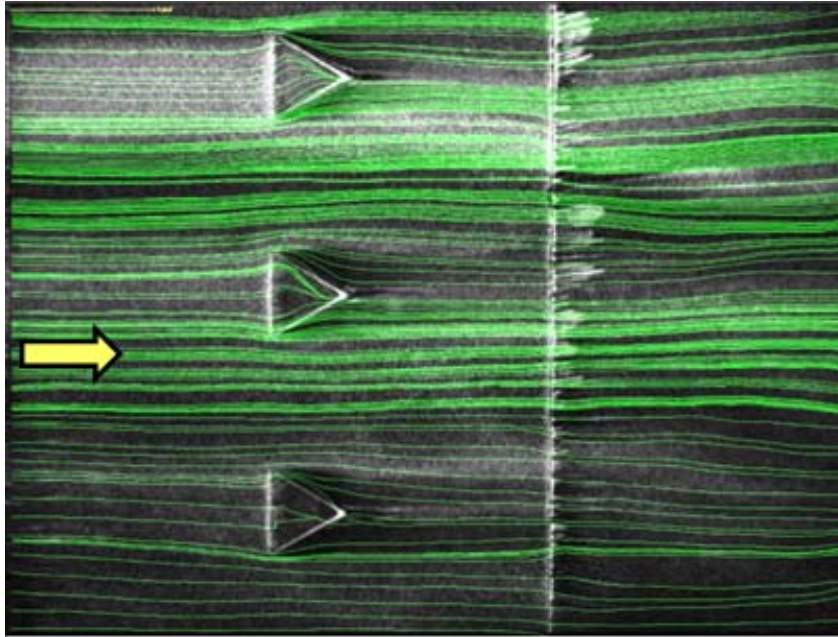
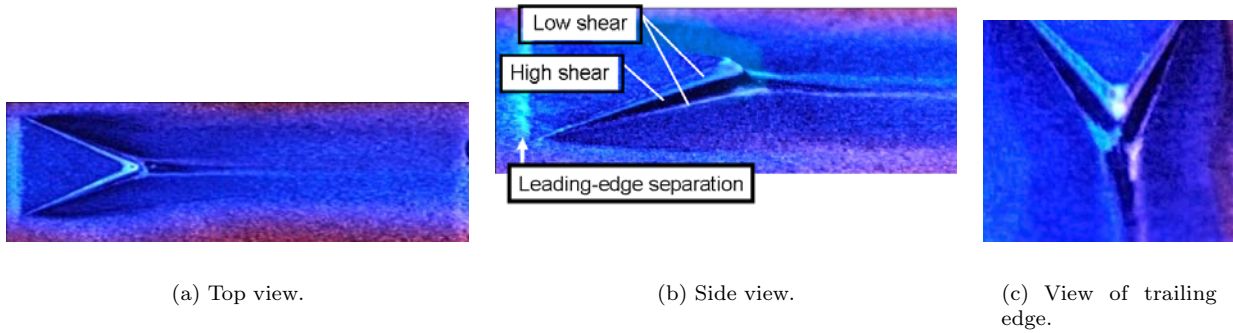


Figure 6. Image processing revealing surface streamlines.



(a) Top view.

(b) Side view.

(c) View of trailing edge.

Figure 7. Enlarged views of surface flow past an MVG.

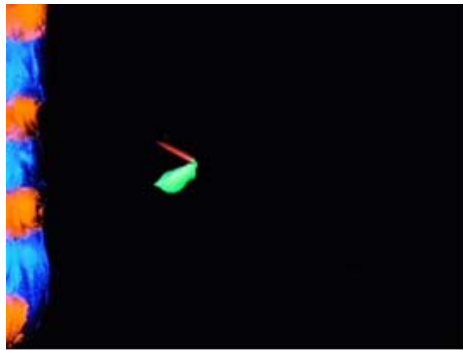
obtaining bright surface visualizations using fluorescent chalk was described. The images were captured by either a still or a video camera. Although the videos were not time resolved, the animated sequences allowed for the detection of minute but critical features in the surface flow which can be connected topologically to the entire flowfield.

Acknowledgments

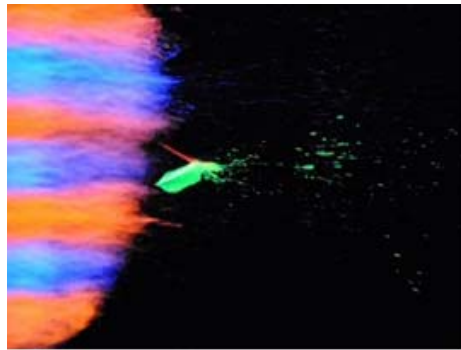
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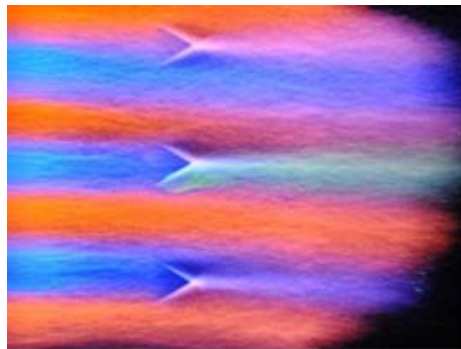
(a) Bands of fluorescent mixture applied ahead of the MVG array and around the sides of an MVG.



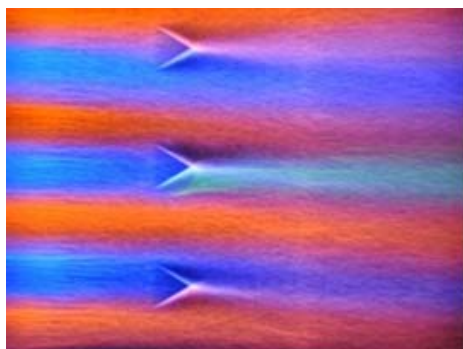
(b) Starting transient.



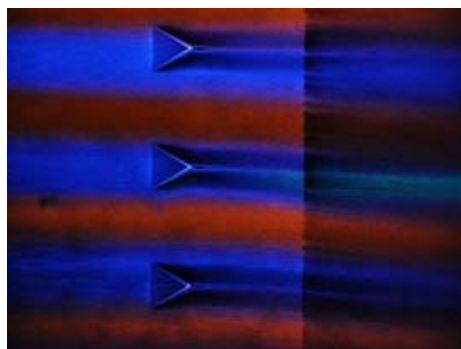
(c) Starting transient 1.3 s after frame b.



(d) Surface flow stabilization, 1.3 s after frame c.

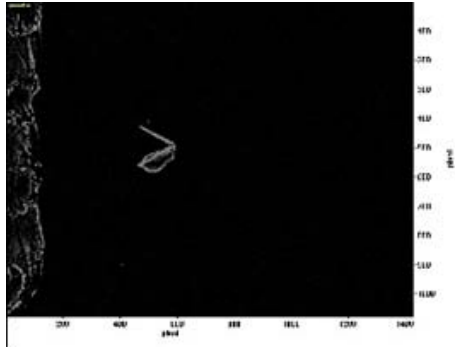


(e) Surface flow stabilization, 1.3 s after frame d.

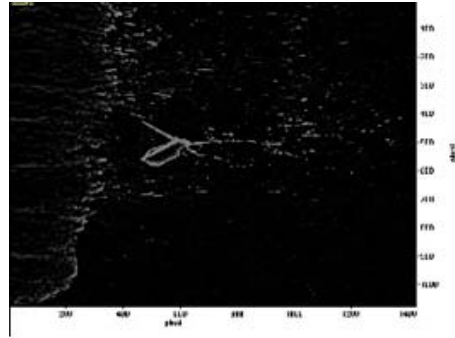


(f) Frame 10 s later, close to shut down.

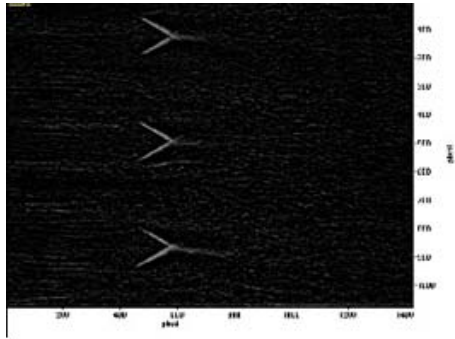
Figure 8. Sample frames of a videoclip showing establishment of surface flow pattern.



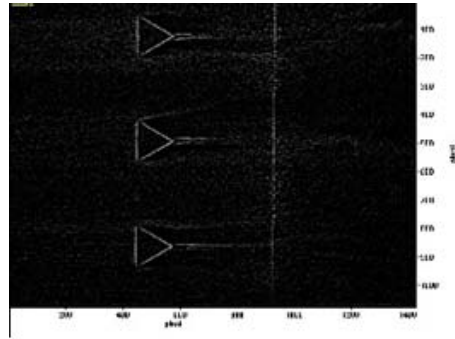
(a) Processed image of Fig. 8(a).



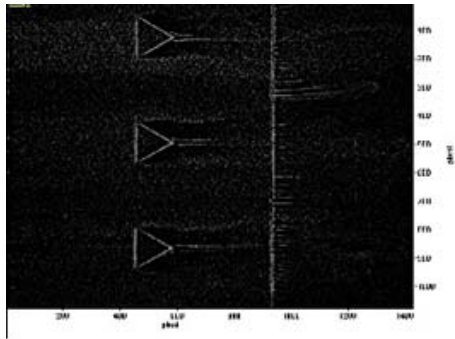
(b) Processed image of Fig. 8(b).



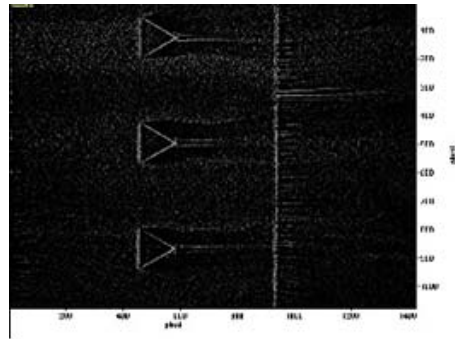
(c) Processed image of Fig. 8(c).



(d) Processed image of Fig. 8(d).



(e) Processed image of Fig. 8(e).



(f) Processed image of Fig. 8(f).

Figure 9. Processed images of Fig. 8.

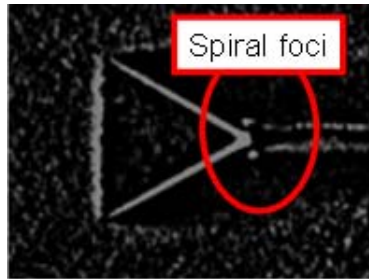


Figure 10. Pair of spiral foci near the trailing edge of an MVG.

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